

4709100090

WELL NO. 11268
SAND BENSON - BALL - SPEER

LOG INTERPRETATION

DEPTH	DENSITY		R _f	NEUTRON				CORE			LOG			PERFORATING DEPTH	
	C/SEC	BULK		INDEX	∅†	Sw	So	So	Sw	∅	∅	Sw	Sg		So
		2.71													
73	450	2.56	100								6	40		73	
74	480	2.53	125								6.5	33		21 HOLES	
75	450	2.56	125								6	42			
76	450	2.56	125								6	42			
77	450	2.56	125								6	42			
78	630	2.42	125								10.5	20			
79	630	2.42	125								10.5	20			
80	630	2.42	125								10.5	20		80	
81	450	2.56	100								6	40			
											7.55	33.92			
												45			
				<u>BALTDOWN</u>											
111	450	2.56	100								4.5	55			
12	540	2.48	125								6.5	33		12	
13	570	2.46	150								7.5	25		12 HOLES 0.45 DIA.	
14	570	2.46	150								7.5	25			
15	570	2.46	150								7.5	25			
16	570	2.46	150								7.5	25			
17	570	2.46	125								7.5	27			
18	540	2.48	100								6.5	35			18
19	450	2.56	100								4.5	55			
											6.61	37	33.86		
				Upper <u>SPEECHLEY</u>											
2834	450	2.56	100								4.5	55			
35	450	2.56	125								4	52			
36	450	2.56	125								4	52			
37	480	2.53	150								5	40			
38	480	2.53	200								5	33		38	
39	510	2.51	200								5.5	28		8 HOLES 1.45 DIA.	
40	540	2.48	200								6.5	25			
41	540	2.48	200								6.5	25			
42	510	2.51	150								6	33			42
43	450	2.56	100								4.5	55			
											5.15	59.9			
												24			

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BRI - Res. Speech, DALLT
681244M

$$43560 \times \frac{1696}{x(1-)} \times \frac{813}{x 15.325} \times (460 + \frac{1060}{x}) \times \frac{160}{x} \text{ Ac.} =$$

$$\frac{881920}{7052} \times 125.1$$

Speechley

2838	871,896,960	X .05	X .67	=	29,209
39		X .055	X .72	=	34527
40		X .065	X .75	=	42505
41		X .065	X .75	=	42505
2842		X .06	X .67	=	183796 35050

Dalltown

3112		X .065	X .67	=	37971
13		X .075	X .75	=	—
14		X .075	X .75	=	—
15		X .075	X .75	=	196176
16		X .075	X .75	=	—
17		X .075	X .75	=	47736
3118		X .065	X .65	=	318721 36838

Newton

4073		X .06	X .60	=	31388
4074		X .065	X .67	=	37971
4075-77		X .06	X .58 X3'	=	91026
4078-80		X .105	X .80 X3'	=	219717
4081		X .06	X .60	=	41199 31388

914,007 MCF

NC

(600)

GL = .625 x 3460 = 2163

Wellhead * = 1560 + 15 = 1575

Res. Press. 1696

Gv. = .625^E

Pcr. = 671

Tcr. = 367

Pr. = $\frac{1696}{671} = 2.53$

Tr = $\frac{566}{367} = 1.54$

Z = .813