WR-35 Rev (9-11)

State of West Virginia Department of Environmental Protection Office of Oil and Gas Well Operator's Report of Well Work

DATE:	October 30, 2013
API#:	47-103-02695

REVISED FOR COMPLETION

							COMPLETI
Farm name:	Weekley	, Larry I. & Donna S.		Operator We	ell No.:	Weekley #8H	 -
LOCATION: Eleg	ation:	727'		_ Quadrangle:	Po	orters Falls	
District:		Green		County:	w	etzel	
	12,170 le 8,000	Feet South of		37 Min	nSec		
Longitut	<u> e, </u>	Feet West of_	80 Deg	. <u>45</u> Mir	nSec	.	
Company:	Stone E	nergy Corpor	ation			•	
Address:		mpton Center		Casing & Tubing	Used in drilling	Left in well	Cement fill up Cu. Ft.
	Morgant	own, WV 265	05	20"	95'	95'	GTS
Agent:	Tim McG	Gregor		13.375"	692'	692'	843 - CTS
Inspector:	Derek Ha	aught		9.625"	2,177'	2,177'	945 - CTS
Date Perm	it Issued: 8/	/10/2011		5.5"		11,509'	2,755
Date Well	Work Comm	enced: 9/29/201	1	2.875"		6,942'	
Date Well	Work Compl	leted: 8/12/20	12				
Verbal Plu	gging:			15	s Plug Back fr	m 2,985' to 1,	800'
Date Perm	ission granted	d on:		2r	od Plug Back fr	om 2,300' to 1,	,800'
Rotary 🗸	Cable	Rig			See Details	on Page Two	
Total Ver	rtical Depth ((ft): 6,464					
Total Mea	sured Depth	(ft): 11,509					
Fresh Wa	ter Depth (ft.): 105					
Salt Wate	r Depth (ft.):	817					
Is coal bein	g mined in a	rea (N/Y)? No					
Coal Depth	s (ft.): ⁵⁸⁷						
Void(s) end	ountered (N	Y) Depth(s) N/A	\				
Producing for Gas: Initial op Final open Time of op	mationen flow49 flow4,250 en flow betw	e than two produc Marcellus MCF/d Oil: In MCF/d Fin Meen initial and fin seen psig (surface	Pay a nitial open fl al open flow al tests_	zone depth (ft) 6 ow 0 B v 0 Bb 223 Hours	7,107' TO 11,435' bl/d bl/d	ta on separate sh	neet)
Second produc	ring formatic	on	D	no dough (A)			
Gas: Initial op	en flow	MCF/d Oil: In	ray zoi itial open fl	ow Bl	bl/d		EIVED
Final open	flow	MCF/d Fina	al open flow	/Bb	1/d	REU	EIVED Oil and Gas
		een initial and fin				Office of	
Static fock PTe	ssure	psig (surface	pressure) af	terHou	rs	DCT	31 2013

I certify under penalty of law that I have personally examined and am familiar with the information submitted on this document and all the attachments and that, based on my inquiry of those individuals immediately responsible for obtaining the information is true, accurate, and complete.

Environment

W. 7 _ 10/30/2013

Were core samples taken? Yes	NoX	Were cut	tings caught	during drilling? Yes_X No	_
Were Electrical, Mechanical or Geoph and CBL	ysical logs recorded on the	his well? If ye	es, please list	t MWD Gamma Ray, Mud Log,	_
FRACTURING OR STIMULATIN	IG, PHYSICAL CHANG CORD OF THE TOPS	GE, ETC. 2). AND BOT	THE WELL TOMS OF	OF PERFORATED INTERVAL L LOG WHICH IS A SYSTEMATI ALL FORMATIONS, INCLUDIN EPTH.	Ć
Perforated Intervals, Fracturing, or Sti	mulating:				
Perforated 17 intervals from 11,435' to 7	7,107'. Performed 17 indi	vidual stages o	of slick water	r stimulation using 5,921,867 gals fresh	
water, Sand - 698,200 lbs 100 Mesh an	d 6,066,860 lbs 40/70. Av	vBDP = 6,362	psi, AvTP = 1	7,307 psi, AvMTP = 9,041 psi,	_
AvinjRate = 81.5 bpm, and AviSIP = 4,1	31 psi.				_
See Attachment for FracFocus informat	on.				<u> </u>
Plug Back Details Including Plug Type	e and Depth(s): 1st kick	off plug from	2,985' to 2,	,104' pumped 3/13/2012. Set with	_
380 sacks Class H (@ 15.8 ppg) ce					et
with 196 sacks Class A (@ 16.0 ppg	ı) cement.				_
Formations Encountered: Surface:	Top Dep	pth	/	Bottom Depth	
See attached sheet for formatio	ns encountered and	their depth	S.		_
					<u> </u>
					_
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				Office of Oil and Ga	<u>-</u> s
				OCT 31 7013	_
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				Environmental Prote 01/10/2	

WEEKLEY #8H API 47-103-02695 Stone Energy Corporation

Horizontal Top Top (ft Bottom (ft Bottom (ft (ft TVD) MD) TVD) MD) Sandstone & Shale Surface 587 FW @ 105' **Pittsburgh Coal** 587 592 Sandstone & Shale 592 1992 SW @ 817' Little Lime 1680 1710 **Big Lime** 1710 1810 Big Injun 1810 1868 Sandstone & Shale 1686 2340 Berea sandstone 2340 2351 Shale 2351 2538 Gordon 2538 2543 **Undiff Devonian Shale** 2543 5685 5820 Rhinestreet 5685 5820 6115 6290 Cashaqua 6115 6290 6228 6438 Middlesex 6228 6438 6252 6474 **West River** 6252 6474 6318 6582 Geneseo 6318 6582 6344 6634 **Tully limestone** 6344 6634 6376 7002 Hamilton 6376 7002 6418 6820

6820

11509

6464

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Office of Oil and Gas

OCT 31 2013

WV Department of Environmental Protection 01/10/2014

^{*} From Pilot Hole Log and Driller's Log

[~] From MWD Gamma Log

Hydraulic Fracturing Fluid Product Component Information Disclosure

103-02695

7/1/2012	Frecture Date:
West Virginia	State:
Wetzel County	County/Parish:
4710302695	API Number:
Stone Energy	Operator Name:
Weekley 8H	Well Name and Number:
-80.77836	Longitude:
39.59167	Latitude:
NAD27	Long/Lat Projection:
Gas	Production Type:
6465	True Vertical Depth (TVD):
5921867	Total Water Volume (gal)*:

Hydraulic Fracturing Fluid Composition

Trade Name	Supplier	Purpose	ingredients	Chemical Abstract Service Number (CAS #)	in Additive	in HE Fluid	Comments
YF100, Slickwater	Schlumberger	Corrosion Inhibitor, Bactericide, Scale Inhibitor, Surfactant, Acid, Breaker, Gelling Agent, Friction Reducer, Iron Control Agent, Clay Control Agent, Fluid Loss Additive, Propping	Water (Including Mix Water Supplied by Client)*		1% by mass)**	87.20622%	
			Crystalline silica	14808-60-7	98.82731%	12.64374%	
			Hydrochloric acid	7647-01-0	0.69865%	0.08938%	
			Ammonium sulfate	Proprietary	0.18070%	0.02312%	
			Carbohydrate polymer	Proprietary	0.17174%	0.02197%	
			Polyethylene glycol monohexyl ether	31726-34-8	0.05437%	0.00696%	
		A. Table	Glutaraldehyde	111-30-8	0.04538%	0.00581%	
			Amine derivative	Proprietary	0.01657%	0.00212%	
			Diammonium peroxidisulphate	7727-54-0	0.01168%	0.00149%	
			Calcium chloride	10043-52-4	0.01082%	0.00138%	
			Trisodium ortho phosphate	7601-54-9	0.00463%	0.00059%	
			Ethane-1,2-diol	107-21-1	0.00463%	0.00059%	
			Sodium erythorbate	6381-77-7	0.00343%	0.00044%	-
			Methanol	67-56-1	0.00244%	0.00031%	
			Aliphatic acids	Proprietary	0.00183%	0.00023%	
			Aliphatic alcohols, ethoxylated #2	Proprietary	0.00183%	0.00023%	
			Prop-2-yn-1-ol	107-19-7	0.00061%	0.00008%	

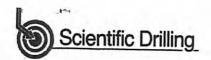
^{*} Total Water Volume sources may include fresh water, produced water, and/or recycled water

Report ID: RPT-8827 (Generated on 11/30/2012 10:28 AM)

All component information listed was obtained from the supplier's Material Safety Data Sheets (MSDS). As such, the Operator is not responsible for inaccurate and Health Administration's (OSHA) regulations govern the criteria for the disclaration. and Health Administration's (OSHA) regulations govern the criteria for the disclosure of this information. Please note that Federal Law protects "proprietary", "trade secret", and "confidential business information" and the criteria for how this information is reported on an MSDS is subject to 29 CFR 1910 1200() and

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^{**} Information is based on the maximum potential for concentration and thus the total may be over 100%





Company: Project:

Stone Energy

Site:

Mary Prospect Weekley Pad

Well:

Weekley et al Unit 1 #8H

Wellbore:

ST02

Design:

ST02 As Drilled

Local Co-ordinate Reference:

TVD Reference:

MD Reference:

North Reference:

Survey Calculation Method:

Database:

Well Weekley et al Unit 1 #8H - Slot W#8HST02

Saxon 141 @ 745.0usft (18' DF + 727' GL)

Saxon 141 @ 745.0usft (18' DF + 727' GL)

Minimum Curvature

EDM-Chris Testa

Project

Mary Prospect, West Virginia

Map System:

US State Plane 1927 (Exact solution)

Geo Datum: Map Zone:

NAD 1927 (NADCON CONUS) West Virginia North 4701

System Datum:

Mean Sea Level

Site

Weekley Pad

Site Position:

From:

Мар

Northing:

400,129.69 usft 1,639,770.43 usft

Latitude:

Longitude:

39° 35' 29,589 N 80° 46' 41.837 W

Position Uncertainty:

0.0 usft

Easting: Slot Radius:

13-3/16 "

Grid Convergence:

-0.82

Well Weekley et al Unit 1 #8H - Slot W#8HST02

Well Position

+E/-W

0.0 usft 0.0 usft

Northing:

Easting:

400,171.63 usft

Latitude: 1,639,751.04 usft

Longitude:

39° 35' 30.000 N

80° 46' 42.092 W

Position Uncertainty

0.0 usft

Wellhead Elevation:

Ground Level:

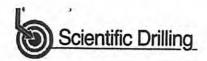
727.0 usft

lagnetics	Model Name	Sample Date	Declination (°)	Dip Angle (°)	Field Strength (nT)
	IGRF2010	03/21/12	-8.46	67.26	52,730

Design	ST02 As Dr	illed				SHOW THE PROPERTY AND SHOWN
Audit Notes: Version:	1.0	Phase:	ACTUAL	Ti- O- D- II	THE RESERVE THE PARTY OF THE PA	
		rilase.	ACTUAL	Tie On Depth:		0.0
Vertical Section:		Depth From (TVD) (usft)	+N/-S (usft)	+E/-W (usft)	Direction (*)	
			0.0	0.0	337	7.85

Survey Program		Date 04/13/12		
From (usft)	To (usft)	Survey (Wellbore)	Tool Name	Description
100.0 4,439.0		4.0 SDI Keeper Gyro (ST02) 9.0 SDI MWD (ST02)	SDI Standard Keeper 103 MWD SDI	SDI Standard Wireline Keeper ver 1.0.3 MWD - Standard ver 1.0.1

y	The state of the s			THE REPORT OF THE REAL PROPERTY.					
Measured Depth (usft)	Inclination (°)	Azimuth	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (*/100usft)	Turn Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
100.0	0.56	232.37	100.0	-0.3	-0.4	-0.1	0.56	0.56	0.00
200.0	0.42	194.31	200.0	-1.0	-0.9	-0.6	0.35	-0.14	-38.06
300.0	0.38	193.32	300.0	-1.6	-1.0	-1.1	0.04	-0.04	-0.99
400.0	0.20	181.81	400.0	-2.1	-1.1	-1.6	0.19	-0.18	-11.51
500.0	0.16	187.81	500.0	-2.4	-1.1	-1.8	0.04	-0.04	6.00
600.0	0.16	216.24	600.0	-2.7	-1.2	-2.0	0.08	0.00	28.43
700.0	0.28	213.20	700.0	-3.0	-1.5	-2.2	0.12	0.12	-3.04
800.0	0.32	218.19	800.0	-3.4	-1.8	-2.5	0.05	0.04	4 99
900.0	0.33	158.49	900.0	-3.9	-1.8	-2.9	0.32	0.01	01/10/201





Company: Project: Site:

Stone Energy Mary Prospect Weekley Pad

Weekley et al Unit 1 #8H

Wellbore: Design:

Well:

ST02

ST02 As Drilled

Local Co-ordinate Reference:

TVD Reference:

MD Reference: North Reference:

Survey Calculation Method:

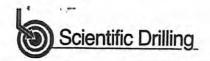
Database:

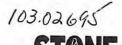
Well Weekley et al Unit 1 #8H - Slot W#8HST02 Saxon 141 @ 745.0usft (18' DF + 727' GL)

Saxon 141 @ 745.0usft (18' DF + 727' GL)

Minimum Curvature **EDM-Chris Testa**

Measured Depth	Inclination	Azimuth	Vertical Depth	+N/-S	+E/-W	Vertical Section	Dogleg Rate	Build Rate	Turn Rate
(usft)	(°)	(°)	(usft)	(usft)	(usft)	(usft)	(°/100usft)	(°/100usft)	(°/100usft)
1 000 0	0.40	405.77	4 000 0	-744	- 12				Land St
1,000.0	0.19	185.77	1,000.0	-4.4	-1.7	-3.4	0.18	-0.14	27.28
1,100.0 1,200.0	0.48	180.83	1,100.0	-4.9	-1.8	-3,9	0.29	0.29	-4.94
1,300.0	0.58 0.53	208.99	1,200.0	-5.8	-2.0	-4.6	0.28	0.10	28.16
1,400.0		212.76	1,300.0	-6.6	-2.5	-5.2	0.06	-0.05	3.77
1,400.0	0.44	223.05	1,400.0	-7.3	-3.0	-5.6	0.12	-0.09	10.29
1,500.0	0.53	202.92	1,500.0	-8.0	-3.5	-6.1	0.19	0.09	-20.13
1,600.0	0.64	201.72	1,600.0	-8.9	-3.9	-6.8	0.11	0.11	-1.20
1,700.0	0.94	197.89	1,700.0	-10.2	-4.3	-7.9	0.30	0.30	-3.83
1,800.0	1.18	209.21	1,799.9	-11.9	-5.1	-9.1	0.32	0.24	11.32
1,900.0	1.17	204.11	1,899.9	-13.8	-6.0	-10.5	0.11	-0.01	-5.10
2,000.0	0.92	187.44	1,999.9	-15.5	-6.5	-11.9	0.39	-0.25	-16.67
2,100.0	0.97	154.90	2,099.9	-17.0	-6.3	-13.4	0.53	0.05	-32.54
2,200.0	2.64	127.32	2,199.9	-19.3	-5.1	-15.9	1.84	1.67	-27.58
2,300.0	6.75	85.60	2,299.5	-20.5	3.1	-20.1	5.09	4.11	-41.71
2,400.0	8.18	63.53	2,398.5	-16.9	16.3	-21.8	3.18	1.42	-22.08
2,500.0	7.93	52.32	2,497.5	-8.9	28.0	-18.8	1.59	-0.25	-11.21
2,600.0	7.35	59.99	2,596.6	-1.5	38.9	-16.0	1.17	-0.58	7.68
2,700.0	6.68	56.15	2,695.9	4.8	49.4	-14.2	0.82	-0.58	-3.85
2,800.0	7.41	57.52	2,795.1	11.5	59.6	-11.8	0.76	0.74	1.37
2,900.0	7,30	54.42	2,894.3	18.7	70.5	-9.2	0.41	-0.11	-3.10
3,000.0	8.29	51.70	2 002 2	26.7	04.5		4.00		
3,100.0	9.21		2,993.3	26.7	81.5	-6.0	1.06	0.99	-2.72
3,200.0	9.52	46.05 43.09	3,092.2	36.8	92,9	-0.9	1.26	0.92	-5.66
3,300.0	10.83	41.00	3,190.8 3,289.3	48.4	104.2	5.5	0.57	0.30	-2.95
3,400.0	10.64			61.6	116.0	13.3	1.37	1.31	-2.10
3,400.0	10.04	41.68	3,387.5	75.7	128.4	21.7	0.23	-0.19	0.68
3,500.0	11.23	40.59	3,485.7	89.9	140.9	30.2	0.62	0.59	-1.09
3,600.0	12.11	38.81	3,583.6	105.4	153.8	39.7	0.95	0.88	-1.78
3,700.0	12.86	37.25	3,681.3	122.3	167.1	50.3	0.82	0.75	-1.56
3,800.0	14.04	34.73	3,778.6	141.1	180.7	62.6	1.32	1.18	-2.53
3,900.0	15.66	33,28	3,875.2	162.3	194.9	76.8	1.66	1.62	-1.44
4,000.0	16.83	30.97	3,971.2	186.0	209.9	93.2	1.34	1.17	-2.32
4,100.0	18.00	28.65	4,066.6	212.0	224.8	111,6	1.36	1.17	-2.31
4,200.0	19.27	28.72	4,161.3	240.3	239.9	132.1	1.27	1.27	0.07
4,300.0	19.50	30.62	4,255.6	269.1	256.6	152.6	0.67	0.23	1.90
4,400.0	19.62	28.24	4,349.9	298.4	272.9	173.5	0.81	0.12	-2.38
4,500.0	19.61	27.55	4,444.0	328.1	288.6	195.1	0.23	-0.01	-0.69
4,600.0	18.31	29.39	4,538.6	356.6	304.2	215.6	1.43	-1.30	1.85
4,700.0	17.50	28.66	4,633.8	383.3	319.1	234.7	0.84	-0.81	-0.73
4,800.0	18.42	29.62	4,729.0	410.2	334.1	253.9	0.96	0.92	0.96
4,900.0	19.03	29.06	4,823.7	438.1	349.8	273.9	0.64	0.92	-0.57
5,000.0	10.76	20.02	4.047.0	467.0	200.0	2010			
5,100.0	19.76 18.67	29.92 29.24	4,917.9	467.2	366.3	294.6	0.78	0.73	0.87
5,200.0	19.30	28.48	5,012.4 5,107.0	495.7 524.0	382,5 398,1	315.0 335.2	1.11 0.67	-1.09 0.63	-0.68 -01/197/2





STANE

Company: Project: Site: Stone Energy Mary Prospect

Weekley Pad Weekley et al Unit 1 #8H

Well: Wellbore:

ST02

Design: ST02 As Drilled

Local Co-ordinate Reference:

TVD Reference: MD Reference:

North Reference:

Survey Calculation Method:

Database:

Well Weekley et al Unit 1 #8H - Slot W#8HST02

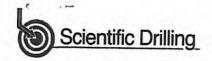
Saxon 141 @ 745.0usft (18' DF + 727' GL) Saxon 141 @ 745.0usft (18' DF + 727' GL)

Grid

Minimum Curvature

EDM-Chris Testa

Measured			Vertical	10000		Vertical	Dogleg	Build	Turn
Depth (usft)	Inclination (°)	Azimuth (°)	Depth (usft)	+N/-S (usft)	+E/-W (usft)	Section (usft)	Rate (°/100usft)	Rate (°/100usft)	Rate (°/100usft)
5,300.0	20.45	30.27	5,201.0	553.6	415.0	356.3	1.30	1.15	1.79
5,400.0	21.17	28.47	5,294.5	584.5	432.5	378.4	0.96	0.72	-1.80
5,500.0	21.13	28.51	5,387.8	616.3	449.7	401.3	0.04	-0.04	0.04
5,600.0	20.96	29.69	5,481.1	647.6	467.3	423.7	0.46	-0.18	1.18
5,700.0	20.67	29.24	5,574.5	678.7	484.6	445.9	0.32	-0.28	-0.45
5,800.0	20.01	29.47	5,668.3	708.9	501.6	467.5	0.67	-0.67	0.23
5,900.0	20.25	30.04	5,762.3	738.7	518.6	488.7	0.31	0.24	0.57
6,000.0	20.81	24.42	5,855.9	769.6	535.4	511.0	2.05	0.57	-5.62
6,100.0	23.73	3.73	5,948.6	806.1	542.9	542.0	8.32	2.92	-20.68
6,200.0	28.94	358.69	6,038.4	850,0	544.2	582.1	5.66	5.21	-5.04
6,300.0	35.65	351.60	6,122.9	903.1	539.5	633.1	7.69	6.71	-7.09
6,400.0	42.61	347.01	6,200.5	965.0	527.7	694.8	7.54	6,96	-4.59
6,500.0	50.23	344.70	6,269.0	1,035.5	509.9	766.8	7.80	7.62	-2.31
6,600.0	57.97	340.86	6,327.6	1,112.8	486.0	847.5	8.34	7.74	-3.84
6,700.0	65.41	336.25	6,375.3	1,194.6	454.1	935.2	8.48	7.44	-4.62
6,800.0	71.87	334.59	6,411.7	1,279.1	415.2	1,028.2	6.64	6.46	-1.66
6,900.0	79.94	333.94	6,435.9	1,366.4	373.0	1,125.0	8.09	8.07	-0.64
7,000.0	88.32	330.76	6,445.7	1,454.4	326.8	1,223.9	8.96	8.38	-3.18
7,100.0	89.73	330.26	6,446.9	1,541.3	277.3	1,323.1	1.49	1.41	-0.50
7,200.0	89.67	330.14	6,447.2	1,628.1	227,7	1,422.2	0.13	-0.06	-0.12
7,300.0	89.74	329.78	6,447.5	1,714.8	177.7	1,521.2	0.37	0.07	-0.36
7,400.0	89.42	328.85	6,448.4	1,800.8	126.7	1,620.1	0.98	-0.32	-0.93
7,500.0	89.57	328.05	6,449.0	1,886.1	74.5	1,718.8	0.81	0.15	-0.80
7,600.0	89,83	327.93	6,449.5	1,970.8	21.4	1,817.3	0.29	0.26	-0.12
7,700.0	89.12	326.93	6,450.2	2,055.3	-32.1	1,915.7	1.23	-0.72	-1.00
7,800.0	89.41	326.02	6,451.4	2,138.6	-87.3	2,013.7	0.96	0.30	-0.91
7,900.0	89.91	326.00	6,452.2	2,221.4	-143.4	2,111.6	0.49	0.49	-0.02
8,000.0	90,93	325,90	6,451.0	2,304.6	-198.9	2,209.5	1.03	1.03	-0.10
8,100.0	89.90	324.47	6,450.4	2,386.5	-256.2	2,307.0	1.77	-1.03	-1.43
8,200.0	90.19	324.50	6,449.9	2,468.0	-314.2	2,404.3	0.29	0.29	0.03
8,300.0	89.94	324.60	6,449.7	2,549.4	-372.3	2,501.6	0.26	-0.24	0.10
8,400.0	88.44	324.86	6,451.0	2,631.1	-430.0	2,599.0	1.52	-1,50	0.26
8,500.0	87.94	325.23	6,454.5	2,712.9	-487.4	2,696.4	0.63	-0.50	0.37
8,600.0	88.78	325.39	6,457.3	2,795.2	-544.1	2,794.0	0.85	0.84	0.16
8,700.0	88.73	325.97	6,459.7	2,877.8	-600.3	2,891.8	0,59	-0.05~	EIVE 0.58
0.008,8	88.20	326.97	6,462.4	2,961.1	-655.7	2,989.8	1.14	-0.53	011 001-00325
8,900.0	89.02	328.07	6,464.9	3,045.4	-709.3	3,088.1	1.37	Office en	Oil anti Gas
9,000.0	89.72	327.92	6,465.6	3,130.3	-762.2	3,186.7	0.72	8.717	3 1 70-0316
9,100.0	89.33	327.93	6,466.7	3,215.0	-815.4	3,285.1	0.40	-b!40 l	0.01
9,200.0	90.27	329.05	6,466.7	3,300,3	-867.5	3,383.8	1.46	0.94	1.12
9,300.0	89.16	328.95	6,467.1	3,386.1	-918.9	3,482.7	1.11	W/1.11	1.12 partno.6611 0 outal pozolec
9,400.0	89.88	328.66	6,468.1	3,471.6	-970.7	3,581.4	0.78	7 0.72 Environiti	ental pisoloc
9,500.0	89.85	327.63	6,468.2	3,556.6	-1,023.4	3,680.0	1.04	-0.03	01/10/201



103.02695



Company: Project: Site: Stone Energy Mary Prospect

Weekley Pad

Well: Weekley et al Unit 1 #8H

Wellbore: Design:

ST02

ST02 As Drilled

Local Co-ordinate Reference:

TVD Reference: MD Reference:

North Reference:

Survey Calculation Method:

Database:

Well Weekley et al Unit 1 #8H - Slot W#8HST02 Saxon 141 @ 745.0usft (18' DF + 727' GL)

Saxon 141 @ 745.0usft (18' DF + 727' GL)
Saxon 141 @ 745.0usft (18' DF + 727' GL)

Grid

Minimum Curvature

EDM-Chris Testa

Measured Depth (usft)	Inclination	Azimuth	Vertical Depth (usft)	+N/-S	+E/-W	Vertical Section	Dogleg Rate	Build Rate	Turn Rate
	ar to be a facility	(°)	(usit)	(usft)	(usft)	(usft)	(*/100usft)	(°/100usft)	(*/100usft)
9,600.0	91.08	327.72	6,467.7	3,640.9	-1,077.2	3,778.4	1.23	1.23	0.09
9,700.0	91.03	327.38	6,465.2	3,725.4	-1,130.5	3,876.8	0.34	-0.04	-0.34
9,800.0	90.17	326.65	6,464.7	3,809.2	-1,185.2	3,974.9	1.13	-0.86	-0.73
9,900.0	89.85	326.06	6,464.8	3,892.4	-1,240.6	4,072.9	0.67	-0.32	-0.59
10,000.0	89.75	325.46	6,465.1	3,975.1	-1,296.9	4,170.7	0.61	-0.11	-0.60
10,100.0	89.80	325.08	6,465.9	4,057.1	-1,354.1	4,268.2	0.38	0.05	-0.38
10,200.0	89.48	325.47	6,466.3	4,139.3	-1,411.0	4,365.8	0.51	-0.32	0.39
10,300.0	88,99	324.91	6,467.7	4,221.6	-1,467.8	4,463.5	0.75	-0,49	-0.57
10,400.0	89.81	324.66	6,468.6	4,303.2	-1,525.6	4,560.8	0.86	0.82	-0.25
10,500.0	89,41	324.89	6,469.2	4,384.9	-1,583.3	4,658.2	0.46	-0,40	0.23
10,600.0	90.33	324.91	6,469.2	4,466.6	-1,641.0	4,755.7	0.92	0.92	0.02
10,700.0	90.70	325,43	6,468.4	4,548.7	-1,698.1	4,853.2	0.64	0.37	0.52
10,800.0	90.89	327.21	6,466.5	4,631.7	-1,753.8	4,951.1	1.79	0.19	1.78
10,900.0	90.63	327.96	6,465.2	4,716.2	-1,807.2	5,049.5	0.79	-0.26	0.75
11,000.0	89.78	328.83	6,464.9	4,801.4	-1,859.6	5,148.2	1.22	-0.85	0.87
11,100.0	90.33	328.16	6,464.8	4,886.7	-1,911.8	5,246.8	0.87	0.55	-0.67
11,200.0	90.24	328.26	6,464.2	4,971.6	-1,964.7	5,345.4	0.13	-0.09	0.10
11,300.0	89.95	327.84	6,464.0	5,056.4	-2,017.6	5,443.9	0.50	-0.28	-0.41
11,400.0	89.62	327.48	6,464.3	5,140.9	-2,071.1	5,542.4	0.49	-0.33	-0.36
11,500.0	89,43	327,34	6,465.3	5,225.1	-2,125.0	5,640.7	0.24	-0.19	-0.14
11,509.0	89.43	327.34	6,465.3	5,232.7	-2,129.9	5,649.5	0.00	0.00	0.00

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Checked By:	Approved By:	Date:	