

WR-35
Rev (9-11)

State of West Virginia
Department of Environmental Protection
Office of Oil and Gas
Well Operator's Report of Well Work

DATE: October 30, 2013
API #: 47-103-02689

**REVISED FOR
COMPLETION**

Farm name: Weekley, Larry I. & Donna S. Operator Well No.: Weekley #2H

LOCATION: Elevation: 727' Quadrangle: Porters Falls

District: Green County: Wetzel
Latitude: 12,200 Feet South of 39 Deg. 37 Min. 30 Sec.
Longitude 8,020 Feet West of 80 Deg. 45 Min. 00 Sec.

Company: Stone Energy Corporation

| Address: | Casing & Tubing | Used in drilling | Left in well | Cement fill up Cu. Ft. |
|--|-----------------|------------------|----------------|------------------------|
| <u>6000 Hampton Center, Suite B Morgantown, WV 26505</u> | <u>20"</u> | <u>75'</u> | <u>75'</u> | <u>GTS</u> |
| Agent: <u>Tim McGregor</u> | <u>13.375"</u> | <u>665'</u> | <u>665'</u> | <u>689 - CTS</u> |
| Inspector: <u>Derek Haught</u> | <u>9.625"</u> | <u>2,190'</u> | <u>2,190'</u> | <u>945 - CTS</u> |
| Date Permit Issued: <u>8/10/2011</u> | <u>5.5"</u> | | <u>10,298'</u> | <u>2,411</u> |
| Date Well Work Commenced: <u>11/28/2011</u> | <u>2.375"</u> | | <u>6,944'</u> | |
| Date Well Work Completed: <u>8/22/2012</u> | | | | |
| Verbal Plugging: | | | | |
| Date Permission granted on: | | | | |
| Rotary <input checked="" type="checkbox"/> Cable <input type="checkbox"/> Rig <input type="checkbox"/> | | | | |
| Total Vertical Depth (ft): <u>6,448</u> | | | | |
| Total Measured Depth (ft): <u>10,317</u> | | | | |
| Fresh Water Depth (ft.): <u>80</u> | | | | |
| Salt Water Depth (ft.): <u>1,409</u> | | | | |
| Is coal being mined in area (N/Y)? <u>No</u> | | | | |
| Coal Depths (ft.): <u>578</u> | | | | |
| Void(s) encountered (N/Y) Depth(s) <u>N/A</u> | | | | |

OPEN FLOW DATA (If more than two producing formations please include additional data on separate sheet)

Producing formation Marcellus Pay zone depth (ft) 6,970' to 10,276'

Gas: Initial open flow 410 MCF/d Oil: Initial open flow 0 Bbl/d

Final open flow 4,680 MCF/d Final open flow 0 Bbl/d

Time of open flow between initial and final tests 165 Hours

Static rock Pressure 1,803 psig (surface pressure) after 1 Hours

Second producing formation _____ Pay zone depth (ft) _____

Gas: Initial open flow _____ MCF/d Oil: Initial open flow _____ Bbl/d

Final open flow _____ MCF/d Final open flow _____ Bbl/d

Time of open flow between initial and final tests _____ Hours

Static rock Pressure _____ psig (surface pressure) after _____ Hours

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I certify under penalty of law that I have personally examined and am familiar with the information submitted on this document and all the attachments and that, based on my inquiry of those individuals immediately responsible for obtaining the information, I believe that the information is true, accurate, and complete.

W. J. [Signature]
Signature

Department of Environmental Protection

10/30/2013

103-02689

Were core samples taken? Yes _____ No X

Were cuttings caught during drilling? Yes X No _____

Were Electrical, Mechanical or Geophysical logs recorded on this well? If yes, please list MWD Gamma Ray, Mud Log, and CBL

NOTE: IN THE AREA BELOW PUT THE FOLLOWING: 1). DETAILS OF PERFORATED INTERVALS, FRACTURING OR STIMULATING, PHYSICAL CHANGE, ETC. 2). THE WELL LOG WHICH IS A SYSTEMATIC DETAILED GEOLOGICAL RECORD OF THE TOPS AND BOTTOMS OF ALL FORMATIONS, INCLUDING COAL ENCOUNTERED BY THE WELLBORE FROM SURFACE TO TOTAL DEPTH.

Perforated Intervals, Fracturing, or Stimulating:

Perforated 13 intervals from 10,276' to 6,970'. Performed 13 individual stages of slick water stimulation using 4,500,425 gals fresh water, Sand - 533,011 lbs 100 Mesh and 4,548,824 lbs 40/70. AvBDP = 6,534 psi, AvTP = 7,149 psi, AvMTP = 9,017 psi, AvInjRate = 81.2 bpm, and AvISIP = 4,482 psi.

See Attachment for FracFocus information.

Plug Back Details Including Plug Type and Depth(s): N/A

| Formations Encountered: Surface: | Top Depth | / | Bottom Depth |
|-------------------------------------|-----------|---|--------------|
|-------------------------------------|-----------|---|--------------|

See attached sheet for formations encountered and their depths.

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103-02689

WEEKLEY #2H
 API 47-103-02689
 Stone Energy Corporation

| | Horizontal | | (ft) | Bottom (ft) | |
|-----------------------|--------------|----------|------|-------------|------------|
| | Top (ft TVD) | Top (MD) | | TVD) | MD) |
| Sandstone & Shale | Surface | | * | 578 | FW @ 80' |
| Pittsburgh Coal | 578 | | * | 582 | |
| Sandstone & Shale | 582 | | * | 1992 | SW @ 1409' |
| Little Lime | 1680 | | * | 1710 | |
| Big Lime | 1710 | | * | 1810 | |
| Big Injun | 1810 | | * | 1868 | |
| Sandstone & Shale | 1686 | | * | 2340 | |
| Berea sandstone | 2340 | | * | 2351 | |
| Shale | 2351 | | * | 2538 | |
| Gordon | 2538 | | * | 2543 | |
| Undiff Devonian Shale | 2543 | | * | 5698 | 5704 |
| Rhinestreet | 5698 | 5704 | ~ | 6100 | 6163 |
| Cashaqua | 6100 | 6163 | ~ | 6230 | 6355 |
| Middlesex | 6230 | 6355 | ~ | 6248 | 6385 |
| West River | 6248 | 6385 | ~ | 6317 | 6513 |
| Geneseo | 6317 | 6513 | ~ | 6341 | 6567 |
| Tully limestone | 6341 | 6567 | ~ | 6372 | 6644 |
| Hamilton | 6372 | 6644 | ~ | 6413 | 6784 |
| Marcellus | 6413 | 6784 | ~ | 6448 | 10317 |
| TD | 6448 | 10317 | | | |

* From Pilot Hole Log and Driller's Log

~ From MWD Gamma Log

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Hydraulic Fracturing Fluid Product Component Information Disclosure

103.02689

| | |
|----------------------------|---------------|
| Fracture Date: | 7/1/2012 |
| State: | West Virginia |
| County/Parish: | Wetzel County |
| API Number: | 4710302689 |
| Operator Name: | Stone Energy |
| Well Name and Number: | Weekley 2H |
| Longitude: | -80.77834 |
| Latitude: | 39.59159 |
| Long/Lat Projection: | NAD27 |
| Production Type: | Gas |
| True Vertical Depth (TVD): | 6448 |
| Total Water Volume (gal): | 4500425 |

Hydraulic Fracturing Fluid Composition

| Trade Name | Supplier | Purpose | Ingredients | Chemical Abstract Service Number (CAS #) | Maximum Ingredient Concentration in Additive (% by mass)** | Maximum Ingredient Concentration in HF Fluid (% by mass)** | Comments |
|-------------------|--------------|--|---|--|--|--|----------|
| YF100, Slickwater | Schlumberger | Corrosion Inhibitor, Bactericide, Scale Inhibitor, Surfactant, Acid, Breaker, Gelling Agent, Friction Reducer, Iron Control Agent, Clay Control Agent, Fluid Loss Additive, Propping | Water (Including Mix Water Supplied by Client)* | - | | 87.09800% | |
| | | | Crystalline silica | 14808-60-7 | 98.65500% | 12.72847% | |
| | | | Hydrochloric acid | 7647-01-0 | 0.71409% | 0.09213% | |
| | | | Carbohydrate polymer | Proprietary | 0.33669% | 0.04344% | |
| | | | Ammonium sulfate | Proprietary | 0.18271% | 0.02357% | |
| | | | Polyethylene glycol monohexyl ether | 31726-34-8 | 0.06018% | 0.00776% | |
| | | | Glutaraldehyde | 111-30-8 | 0.04764% | 0.00615% | |
| | | | Diammonium peroxodisulphate | 7727-54-0 | 0.02174% | 0.00281% | |
| | | | Calcium chloride | 10043-52-4 | 0.01075% | 0.00139% | |
| | | | Amine derivative | Proprietary | 0.01035% | 0.00134% | |
| | | | Trisodium ortho phosphate | 7601-54-9 | 0.00517% | 0.00067% | |
| | | | Ethane-1,2-diol | 107-21-1 | 0.00517% | 0.00067% | |
| | | | Sodium erythorbate | 6381-77-7 | 0.00359% | 0.00046% | |
| | | | Methanol | 67-56-1 | 0.00273% | 0.00035% | |
| | | | Aliphatic acids | Proprietary | 0.00205% | 0.00026% | |
| | | | Aliphatic alcohols, ethoxylated #2 | Proprietary | 0.00205% | 0.00026% | |
| | | | Prop-2-yn-1-ol | 107-19-7 | 0.00068% | 0.00009% | |

* Total Water Volume sources may include fresh water, produced water, and/or recycled water

** Information is based on the maximum potential for concentration and thus the total may be over 100%

Report ID: RPT-8824 (Generated on 11/30/2012 10:26 AM)

All component information listed was obtained from the supplier's Material Safety Data Sheets (MSDS). As such, the Operator is not responsible for inaccurate and/or incomplete information. Any questions regarding the content of the MSDS should be directed to the supplier who provided it. The Occupational Safety and Health Administration's (OSHA) regulations govern the criteria for the disclosure of this information. Please note that Federal Law protects "proprietary", "trade secret", and "confidential business information" and the criteria for how this information is reported on an MSDS is subject to 29 CFR 1910.1200(i) and Appendix B.

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| | | | |
|------------------|--------------------------|-------------------------------------|---|
| Company: | Stone Energy | Local Co-ordinate Reference: | Well Weekley et al Unit 1 #2H - Slot W#2H |
| Project: | Mary Prospect | TVD Reference: | Saxon 141 @ 745.0usft (18' RKB + 727' GL) |
| Site: | Weekley Pad | MD Reference: | Saxon 141 @ 745.0usft (18' RKB + 727' GL) |
| Well: | Weekley et al Unit 1 #2H | North Reference: | Grid |
| Wellbore: | Original Well | Survey Calculation Method: | Minimum Curvature |
| Design: | As Drilled | Database: | EDM-Chris Testa |

| | | | |
|--------------------|--------------------------------------|----------------------|----------------|
| Project | Mary Prospect, West Virginia | | |
| Map System: | US State Plane 1927 (Exact solution) | System Datum: | Mean Sea Level |
| Geo Datum: | NAD 1927 (NADCON CONUS) | | |
| Map Zone: | West Virginia North 4701 | | |

| | | | | | |
|------------------------------|-------------|---------------------|-------------------|--------------------------|------------------|
| Site | Weekley Pad | | | | |
| Site Position: | | Northing: | 400,129.69 usft | Latitude: | 39° 35' 29.589 N |
| From: | Map | Easting: | 1,639,770.43 usft | Longitude: | 80° 46' 41.837 W |
| Position Uncertainty: | 0.0 usft | Slot Radius: | 13-3/16 " | Grid Convergence: | -0.82 ° |

| | | | | | | |
|-----------------------------|--------------------------------------|----------|----------------------------|-------------------|----------------------|------------------|
| Well | Weekley et al Unit 1 #2H - Slot W#2H | | | | | |
| Well Position | +N/-S | 0.0 usft | Northing: | 400,142.40 usft | Latitude: | 39° 35' 29.712 N |
| | +E/-W | 0.0 usft | Easting: | 1,639,754.98 usft | Longitude: | 80° 46' 42.036 W |
| Position Uncertainty | 0.0 usft | | Wellhead Elevation: | usft | Ground Level: | 727.0 usft |

| | | | | | |
|------------------|-------------------|--------------------|------------------------|----------------------|----------------------------|
| Wellbore | Original Well | | | | |
| Magnetics | Model Name | Sample Date | Declination (°) | Dip Angle (°) | Field Strength (nT) |
| | IGRF2010 | 03/01/12 | -8.45 | 67.26 | 52,731 |

| | | | | | |
|--------------------------|--------------------------------|---------------------|---------------------|----------------------|-----|
| Design | As Drilled | | | | |
| Audit Notes: | | | | | |
| Version: | 1.0 | Phase: | ACTUAL | Tie On Depth: | 0.0 |
| Vertical Section: | Depth From (TVD) (usft) | +N/-S (usft) | +E/-W (usft) | Direction (°) | |
| | 0.0 | 0.0 | 0.0 | 151.32 | |

| | | | | | |
|-----------------------|------------------|---------------------------------|-------------------------|--|--|
| Survey Program | Date | 03/23/12 | | | |
| From (usft) | To (usft) | Survey (Wellbore) | Tool Name | Description | |
| 100.0 | 5,183.0 | SDI Keeper Gyro (Original Well) | SDI Standard Keeper 103 | SDI Standard Wireline Keeper ver 1.0.3 | |
| 5,237.0 | 10,317.0 | SDI MWD (Original Well) | MWD SDI | MWD - Standard ver 1.0.1 | |

| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
|-----------------------|-----------------|-------------|-----------------------|--------------|--------------|-------------------------|-------------------------|------------------------|-----------------------|
| 0.0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 100.0 | 0.21 | 72.21 | 100.0 | 0.1 | 0.2 | 0.0 | 0.21 | 0.21 | 0.00 |
| 200.0 | 0.21 | 78.95 | 200.0 | 0.1 | 0.5 | 0.1 | 0.02 | 0.00 | 6.74 |
| 300.0 | 0.08 | 92.93 | 300.0 | 0.2 | 0.8 | 0.2 | 0.13 | 0.13 | 13.98 |
| 400.0 | 0.06 | 115.19 | 400.0 | 0.2 | 0.9 | 0.3 | 0.03 | 0.02 | 22.26 |
| 500.0 | 0.04 | 113.13 | 500.0 | 0.1 | 1.0 | 0.4 | 0.02 | -0.02 | -2.06 |
| 600.0 | 0.08 | 130.01 | 600.0 | 0.1 | 1.1 | 0.5 | 0.04 | 0.04 | 16.38 |
| 700.0 | 0.14 | 108.44 | 700.0 | 0.0 | 1.2 | 0.6 | 0.07 | 0.06 | -21.57 |
| 800.0 | 0.45 | 101.65 | 800.0 | -0.1 | 1.7 | 1.0 | 0.31 | 0.31 | 6.78 |
| 900.0 | 0.49 | 94.96 | 900.0 | -0.3 | 2.5 | 1.4 | 0.07 | 0.04 | -6.69 |

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| Wellbore: | Original Well | Survey Calculation Method: | Minimum Curvature |
| Design: | As Drilled | Database: | EDM-Chris Testa |

Survey

| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N-S (usft) | +E-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
|-----------------------|-----------------|-------------|-----------------------|-------------|-------------|-------------------------|-------------------------|------------------------|-----------------------|
| 1,000.0 | 0.24 | 101.39 | 1,000.0 | -0.3 | 3.2 | 1.8 | 0.25 | -0.25 | 6.43 |
| 1,100.0 | 0.51 | 97.66 | 1,100.0 | -0.4 | 3.8 | 2.2 | 0.27 | 0.27 | -3.73 |
| 1,200.0 | 0.45 | 104.87 | 1,200.0 | -0.6 | 4.6 | 2.8 | 0.09 | -0.06 | 7.21 |
| 1,300.0 | 0.44 | 108.63 | 1,300.0 | -0.8 | 5.4 | 3.3 | 0.03 | -0.01 | 3.76 |
| 1,400.0 | 0.48 | 108.68 | 1,400.0 | -1.1 | 6.1 | 3.9 | 0.04 | 0.04 | 0.05 |
| 1,500.0 | 0.36 | 119.74 | 1,500.0 | -1.4 | 6.8 | 4.5 | 0.14 | -0.12 | 11.06 |
| 1,600.0 | 0.51 | 172.25 | 1,600.0 | -2.0 | 7.1 | 5.2 | 0.41 | 0.15 | 52.51 |
| 1,700.0 | 0.43 | 165.34 | 1,700.0 | -2.8 | 7.3 | 5.9 | 0.10 | -0.08 | -6.91 |
| 1,800.0 | 0.35 | 182.37 | 1,800.0 | -3.4 | 7.4 | 6.6 | 0.14 | -0.08 | 17.03 |
| 1,900.0 | 0.36 | 180.81 | 1,900.0 | -4.1 | 7.4 | 7.1 | 0.01 | 0.01 | -1.56 |
| 2,000.0 | 0.07 | 234.81 | 2,000.0 | -4.4 | 7.3 | 7.4 | 0.32 | -0.29 | 54.00 |
| 2,100.0 | 0.09 | 176.45 | 2,100.0 | -4.5 | 7.3 | 7.5 | 0.08 | 0.02 | -58.36 |
| 2,200.0 | 0.11 | 211.35 | 2,200.0 | -4.7 | 7.2 | 7.6 | 0.06 | 0.02 | 34.90 |
| 2,300.0 | 0.73 | 185.44 | 2,300.0 | -5.4 | 7.1 | 8.1 | 0.63 | 0.62 | -25.91 |
| 2,400.0 | 1.82 | 198.83 | 2,399.9 | -7.5 | 6.5 | 9.7 | 1.12 | 1.09 | 13.39 |
| 2,500.0 | 3.33 | 201.57 | 2,499.8 | -11.7 | 5.0 | 12.7 | 1.51 | 1.51 | 2.74 |
| 2,600.0 | 4.44 | 208.00 | 2,599.6 | -17.9 | 2.1 | 16.7 | 1.19 | 1.11 | 6.43 |
| 2,700.0 | 5.20 | 217.02 | 2,699.2 | -24.9 | -2.5 | 20.7 | 1.07 | 0.76 | 9.02 |
| 2,800.0 | 4.83 | 212.47 | 2,798.9 | -32.1 | -7.5 | 24.5 | 0.54 | -0.37 | -4.55 |
| 2,900.0 | 4.68 | 209.92 | 2,898.5 | -39.2 | -11.8 | 28.7 | 0.26 | -0.15 | -2.55 |
| 3,000.0 | 4.95 | 209.56 | 2,998.2 | -46.4 | -15.9 | 33.1 | 0.27 | 0.27 | -0.36 |
| 3,100.0 | 4.91 | 209.93 | 3,097.8 | -53.9 | -20.2 | 37.6 | 0.05 | -0.04 | 0.37 |
| 3,200.0 | 4.13 | 209.25 | 3,197.5 | -60.8 | -24.1 | 41.7 | 0.78 | -0.78 | -0.68 |
| 3,300.0 | 3.67 | 206.93 | 3,297.3 | -66.7 | -27.3 | 45.5 | 0.49 | -0.46 | -2.32 |
| 3,400.0 | 2.82 | 206.30 | 3,397.1 | -71.8 | -29.8 | 48.7 | 0.85 | -0.85 | -0.63 |
| 3,500.0 | 1.90 | 193.97 | 3,497.0 | -75.6 | -31.3 | 51.3 | 1.05 | -0.92 | -12.33 |
| 3,600.0 | 1.11 | 177.60 | 3,597.0 | -78.2 | -31.7 | 53.4 | 0.89 | -0.79 | -16.37 |
| 3,700.0 | 0.77 | 169.88 | 3,697.0 | -79.8 | -31.5 | 54.9 | 0.36 | -0.34 | -7.72 |
| 3,800.0 | 0.37 | 150.53 | 3,797.0 | -80.8 | -31.2 | 55.9 | 0.44 | -0.40 | -19.35 |
| 3,900.0 | 0.43 | 141.38 | 3,897.0 | -81.3 | -30.8 | 56.6 | 0.09 | 0.06 | -9.15 |
| 4,000.0 | 0.43 | 128.26 | 3,997.0 | -81.9 | -30.3 | 57.3 | 0.10 | 0.00 | -13.12 |
| 4,100.0 | 0.44 | 129.15 | 4,096.9 | -82.3 | -29.7 | 58.0 | 0.01 | 0.01 | 0.89 |
| 4,200.0 | 0.27 | 172.30 | 4,196.9 | -82.8 | -29.4 | 58.5 | 0.31 | -0.17 | 43.15 |
| 4,300.0 | 0.20 | 296.78 | 4,296.9 | -83.0 | -29.5 | 58.6 | 0.42 | -0.07 | 124.48 |
| 4,400.0 | 0.28 | 296.50 | 4,396.9 | -82.8 | -29.9 | 58.3 | 0.08 | 0.08 | -0.28 |
| 4,500.0 | 0.23 | 316.83 | 4,496.9 | -82.5 | -30.3 | 57.9 | 0.10 | -0.05 | 20.33 |
| 4,600.0 | 0.30 | 320.25 | 4,596.9 | -82.2 | -30.6 | 57.4 | 0.07 | 0.07 | 3.42 |
| 4,700.0 | 0.27 | 303.11 | 4,696.9 | -81.9 | -30.9 | 57.0 | 0.09 | -0.03 | -17.14 |
| 4,800.0 | 0.14 | 316.72 | 4,796.9 | -81.6 | -31.2 | 56.6 | 0.14 | -0.13 | 13.61 |
| 4,900.0 | 0.19 | 338.56 | 4,896.9 | -81.4 | -31.3 | 56.4 | 0.08 | 0.05 | 21.84 |
| 5,000.0 | 0.34 | 341.17 | 4,996.9 | -81.0 | -31.5 | 55.9 | 0.15 | 0.15 | 2.61 |
| 5,100.0 | 0.30 | 325.66 | 5,096.9 | -80.4 | -31.8 | 55.3 | 0.10 | -0.04 | -15.51 |
| 5,200.0 | 0.55 | 335.88 | 5,196.9 | -79.7 | -32.1 | 54.6 | 0.26 | 0.25 | 10.02 |

01/10/2014

| | | | |
|------------------|--------------------------|-------------------------------------|---|
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| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N-S (usft) | +E-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
|-----------------------|-----------------|-------------|-----------------------|-------------|-------------|-------------------------|-------------------------|------------------------|-----------------------|
| 5,300.0 | 0.29 | 3.18 | 5,296.9 | -79.0 | -32.4 | 53.8 | 0.33 | -0.27 | 27.30 |
| 5,400.0 | 0.12 | 42.05 | 5,396.9 | -78.7 | -32.7 | 53.3 | 0.21 | -0.17 | 38.87 |
| 5,500.0 | 5.68 | 157.30 | 5,496.8 | -82.5 | -30.7 | 57.6 | 5.73 | 5.57 | 115.25 |
| 5,600.0 | 8.90 | 163.03 | 5,596.0 | -94.2 | -26.3 | 70.0 | 3.29 | 3.22 | 5.73 |
| 5,700.0 | 14.78 | 171.98 | 5,693.6 | -115.3 | -22.3 | 90.4 | 6.14 | 5.88 | 8.95 |
| 5,800.0 | 19.49 | 176.12 | 5,789.4 | -143.6 | -19.3 | 116.8 | 4.87 | 4.71 | 4.14 |
| 5,900.0 | 25.17 | 179.31 | 5,881.8 | -181.7 | -17.8 | 150.9 | 5.80 | 5.67 | 3.19 |
| 6,000.0 | 30.76 | 178.54 | 5,970.2 | -228.4 | -17.2 | 192.1 | 5.61 | 5.60 | -0.77 |
| 6,100.0 | 37.26 | 178.59 | 6,053.2 | -284.0 | -15.5 | 241.8 | 6.50 | 6.50 | 0.05 |
| 6,200.0 | 44.07 | 180.28 | 6,129.2 | -349.0 | -14.9 | 299.0 | 6.90 | 6.81 | 1.68 |
| 6,300.0 | 50.31 | 179.77 | 6,197.1 | -422.3 | -15.1 | 363.2 | 6.26 | 6.25 | -0.51 |
| 6,400.0 | 55.53 | 179.84 | 6,256.8 | -502.5 | -15.0 | 433.6 | 5.21 | 5.21 | 0.07 |
| 6,500.0 | 60.22 | 176.60 | 6,310.5 | -586.7 | -13.0 | 508.5 | 5.44 | 4.69 | -3.24 |
| 6,600.0 | 65.54 | 169.47 | 6,356.0 | -674.9 | -1.5 | 591.4 | 8.28 | 5.32 | -7.13 |
| 6,700.0 | 72.41 | 164.16 | 6,391.8 | -765.8 | 19.6 | 681.2 | 8.47 | 6.88 | -5.31 |
| 6,800.0 | 77.86 | 159.01 | 6,417.2 | -857.4 | 50.3 | 776.4 | 7.37 | 5.44 | -5.14 |
| 6,900.0 | 82.86 | 153.92 | 6,434.3 | -948.0 | 88.9 | 874.4 | 7.09 | 5.01 | -5.10 |
| 7,000.0 | 85.69 | 147.91 | 6,443.7 | -1,034.9 | 137.5 | 973.9 | 6.61 | 2.83 | -6.00 |
| 7,100.0 | 88.69 | 145.44 | 6,448.4 | -1,118.0 | 192.8 | 1,073.4 | 3.88 | 2.99 | -2.48 |
| 7,200.0 | 90.74 | 143.54 | 6,449.1 | -1,199.6 | 250.6 | 1,172.7 | 2.79 | 2.05 | -1.90 |
| 7,300.0 | 91.58 | 143.17 | 6,447.1 | -1,279.9 | 310.2 | 1,271.7 | 0.91 | 0.84 | -0.37 |
| 7,400.0 | 92.10 | 142.25 | 6,443.7 | -1,359.4 | 370.7 | 1,370.5 | 1.06 | 0.53 | -0.92 |
| 7,500.0 | 91.02 | 141.30 | 6,441.2 | -1,437.9 | 432.6 | 1,469.1 | 1.45 | -1.09 | -0.96 |
| 7,600.0 | 90.84 | 141.42 | 6,439.6 | -1,515.7 | 495.4 | 1,567.5 | 0.21 | -0.17 | 0.12 |
| 7,700.0 | 90.59 | 143.22 | 6,438.4 | -1,595.0 | 556.3 | 1,666.3 | 1.82 | -0.26 | 1.80 |
| 7,800.0 | 90.32 | 143.96 | 6,437.5 | -1,675.5 | 615.7 | 1,765.4 | 0.78 | -0.27 | 0.73 |
| 7,900.0 | 89.33 | 144.99 | 6,437.8 | -1,756.9 | 673.7 | 1,864.7 | 1.43 | -0.99 | 1.03 |
| 8,000.0 | 89.47 | 145.52 | 6,439.0 | -1,838.8 | 731.1 | 1,964.1 | 0.54 | 0.14 | 0.53 |
| 8,100.0 | 90.10 | 146.99 | 6,439.3 | -1,922.0 | 786.5 | 2,063.7 | 1.60 | 0.63 | 1.48 |
| 8,200.0 | 90.21 | 148.41 | 6,439.0 | -2,006.5 | 840.1 | 2,163.5 | 1.42 | 0.11 | 1.42 |
| 8,300.0 | 90.75 | 149.25 | 6,438.2 | -2,092.1 | 891.6 | 2,263.4 | 1.00 | 0.54 | 0.84 |
| 8,400.0 | 91.17 | 148.78 | 6,436.7 | -2,178.0 | 942.9 | 2,363.3 | 0.63 | 0.41 | -0.48 |
| 8,500.0 | 90.59 | 146.77 | 6,435.2 | -2,262.3 | 996.6 | 2,463.1 | 2.09 | -0.58 | -2.01 |
| 8,600.0 | 90.10 | 146.29 | 6,434.4 | -2,345.9 | 1,051.6 | 2,562.7 | 0.68 | -0.49 | -0.48 |
| 8,700.0 | 89.95 | 144.92 | 6,434.6 | -2,428.4 | 1,108.0 | 2,662.2 | 1.38 | -0.15 | -1.37 |
| 8,800.0 | 89.79 | 144.30 | 6,434.7 | -2,509.8 | 1,166.1 | 2,761.5 | 0.64 | -0.17 | -0.62 |
| 8,900.0 | 89.15 | 143.89 | 6,435.2 | -2,590.8 | 1,224.7 | 2,860.7 | 0.76 | -0.64 | -0.41 |
| 9,000.0 | 88.18 | 143.68 | 6,437.8 | -2,671.5 | 1,283.7 | 2,959.8 | 0.99 | -0.97 | -0.22 |
| 9,100.0 | 88.96 | 142.72 | 6,440.4 | -2,751.4 | 1,343.8 | 3,058.8 | 1.23 | 0.78 | -0.95 |
| 9,200.0 | 89.56 | 141.80 | 6,441.7 | -2,830.5 | 1,405.0 | 3,157.5 | 1.10 | 0.60 | -0.92 |
| 9,300.0 | 90.23 | 141.21 | 6,441.9 | -2,908.8 | 1,467.2 | 3,256.1 | 0.90 | 0.67 | -0.60 |
| 9,400.0 | 91.47 | 141.70 | 6,440.3 | -2,986.7 | 1,529.8 | 3,354.5 | 1.34 | 1.24 | 0.49 |
| 9,500.0 | 91.06 | 142.99 | 6,437.7 | -3,065.9 | 1,590.8 | 3,453.2 | 1.35 | -0.41 | 0.49 |

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| | |
|---------------------------------------|---|
| Company: Stone Energy | Local Co-ordinate Reference: Well Weekley et al Unit 1 #2H - Slot W#2H |
| Project: Mary Prospect | TVD Reference: Saxon 141 @ 745.0usft (18' RKB + 727' GL) |
| Site: Weekley Pad | MD Reference: Saxon 141 @ 745.0usft (18' RKB + 727' GL) |
| Well: Weekley et al Unit 1 #2H | North Reference: Grid |
| Wellbore: Original Well | Survey Calculation Method: Minimum Curvature |
| Design: As Drilled | Database: EDM-Chris Testa |

Survey

| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
|-----------------------|-----------------|-------------|-----------------------|--------------|--------------|-------------------------|-------------------------|------------------------|-----------------------|
| 9,600.0 | 89.33 | 144.99 | 6,437.2 | -3,146.8 | 1,649.7 | 3,552.4 | 2.64 | -1.73 | 2.00 |
| 9,700.0 | 88.26 | 145.14 | 6,439.8 | -3,228.8 | 1,706.7 | 3,651.8 | 1.09 | -1.07 | 0.15 |
| 9,800.0 | 89.39 | 146.10 | 6,441.7 | -3,311.3 | 1,763.2 | 3,751.3 | 1.49 | 1.13 | 0.96 |
| 9,900.0 | 89.34 | 147.74 | 6,442.7 | -3,395.2 | 1,817.7 | 3,851.0 | 1.64 | -0.05 | 1.64 |
| 10,000.0 | 88.19 | 147.64 | 6,444.6 | -3,479.9 | 1,870.9 | 3,950.8 | 1.16 | -1.15 | -0.10 |
| 10,100.0 | 89.49 | 147.51 | 6,446.6 | -3,564.1 | 1,924.7 | 4,050.5 | 1.30 | 1.30 | -0.13 |
| 10,200.0 | 89.71 | 148.34 | 6,447.0 | -3,648.8 | 1,977.8 | 4,150.4 | 0.86 | 0.22 | 0.83 |
| 10,300.0 | 89.26 | 148.11 | 6,448.1 | -3,733.8 | 2,030.5 | 4,250.2 | 0.50 | -0.45 | -0.23 |
| 10,317.0 | 89.26 | 148.11 | 6,448.3 | -3,748.2 | 2,039.5 | 4,267.2 | 0.00 | 0.00 | 0.00 |